

APPENDIX - V : DESIGN EXAMPLE OF CHECK DAM

DESIGN EXAMPLE OF CHECK DAM

Data

Catchment area = 15.68 sq. km (6.127 sq. miles)
Nature of Catchment = Good
Average annual rainfall = 825 mm
65 percent dependable rainfall = 717 mm

Gauge-Discharge Table

Discharge	Water Level
50	89.98
60	91.59
70	93.21
80	94.83
90	96.45
110	99.69
115	100.50

Yield from Catchment

From Strange's Table
Yield/sq. km for 717 mm rainfall is 26.08 percent of rainfall = 0.187 MCM
Yield from the catchment = 15.68×0.187
= 2.93 MCM

Design Flood

Where a formula applicable to a given situation is available viz. Dicken's or Ryve's formula. Assuming that following Dicken's formula is available

$$Q = 1000 A^{3/4}$$
$$Q = 1000 (6.127)^{3/4}$$
$$= 3894 \text{ cusecs}$$
$$= 110.37 \text{ cumecs}$$

Design of Sharp Crested Weir

$$\text{Discharge, } Q = 1.84 (L - KnH) H^{3/2}$$

Where,

L = Length of weir

K = Coefficient of end contraction (adopted 0.1)

n = Number of end contractions (in this case = 2)

H = Total head over spillway crest

Q = Discharge

Providing a total head (including velocity head of 0.05) = 1.05 m

$$\begin{aligned} 110.37 &= 1.84 (L - 0.1 \times 2 \times 1.05) 1.05^{3/2} \\ &= 1.84 (L - 0.21) \times 1.076 \end{aligned}$$

$$L = 55.95 \text{ m}$$

Say 56 m

$$\begin{aligned} \text{Discharge intensity, } q &= \frac{110.37}{56} \\ &= 1.97 \text{ cumecs} \end{aligned}$$

$$\begin{aligned} \text{Normal Scour depth, } R &= 1.35 \left(\frac{q^2}{f} \right)^{1/3} \\ &= 1.35 \left(\frac{1.97^2}{f} \right)^{1/3} \end{aligned}$$

Assuming, $f = 1$

$R = 2.12$ m below the maximum flood level

Computed flood level at weir site corresponding to the design discharge of 110.37 cumecs is 99.75 m

Keeping the crest level = 99.00 m

$$\begin{aligned} \text{Maximum water level} &= 99.00 + 1.05 \\ &= 100.05 \text{ m} \end{aligned}$$

Thus, there will be a net flood lift of $(100.05 - 99.75)$ i.e. 0.3 m at the weir site

$$\begin{aligned} \text{Depth of downstream cutoff} &= 1.5 R \\ &= 1.5 \times 2.12 \\ &= 3.18 \text{ m} \end{aligned}$$

$$\text{Desired R.L. of cut off} = 100.05 - 3.18 = 96.87 \text{ m}$$

Average bed level of deep channel is 97.30 m

Providing a minimum depth of 1 m for cutoff

$$\begin{aligned} \text{Actual R.L. of cutoff} &= 97.30 - 1.00 \\ &= 96.30 \text{ (against the desired level of 96.87)} \end{aligned}$$

Design of Weir Floor

Design flood = 110.37 cumecs

Length of weir = 56 m

Height of weir above the bed = $99.00 - 97.30$
= 1.7 m

Bottom width of weir = 1.6 m

Total maximum head, $H = 1.7$ m

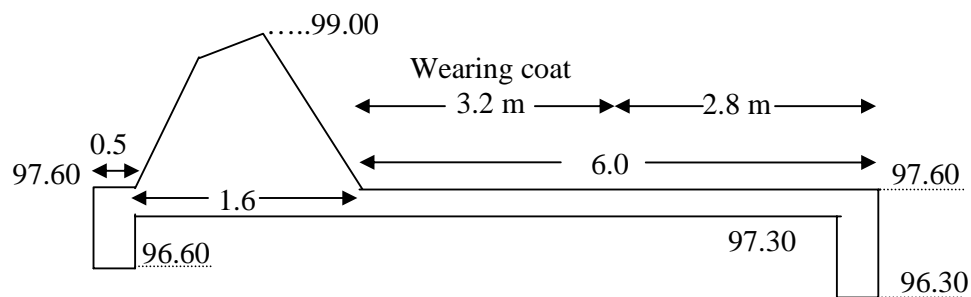
Total creep length required, $L = C \times H$

Adopting $C = 4$

$L = 4 \times 1.7$
= 7.22 m
Say 7.25 m

$$\begin{aligned} \text{Length of downstream floor, } L_d &= 2.21 C \sqrt{\left(\frac{H}{13}\right)} \\ &= 2.21 \times 4 \sqrt{\left(\frac{1.7}{13}\right)} \\ &= 3.19 \text{ m} \\ &\text{Say } 3.20 \text{ m} \end{aligned}$$

Provide a length of 6.0 m and provide wearing coat for 3.20 m.



Bottom level of downstream cutoff = 96.30

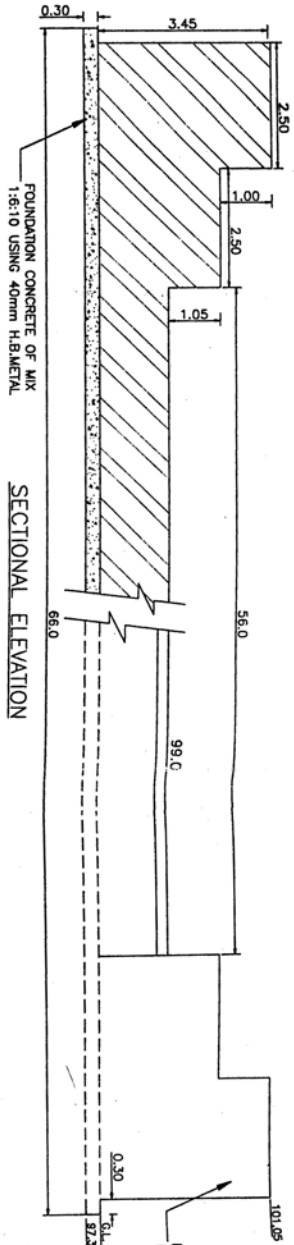
Assuming bottom level of U/S cut off = 96.60

Provide floor thickness = 0.3 m

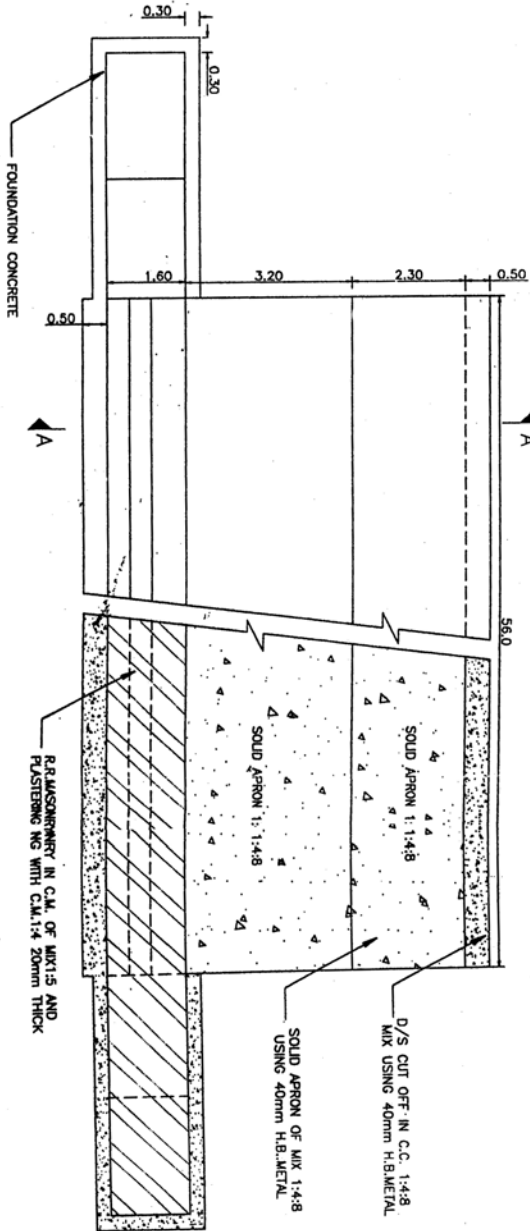
Actual creep length = $1.0 + 0.5 + 1.6 + 3.2 + 2.8 + 1.3 = 10.4$ m against 7.25 m required.
Hence O.k.

The sample drawings for Check Dam are shown in Figure A-5.1.

PLAN SHOWING CHECK DAM



SECTIONAL ELEVATION



HALF PLAN AT TOP AND B) HALF PLAN AT BOTTOM

NOTE:-- ALL DIMENSIONS ARE IN METRES.

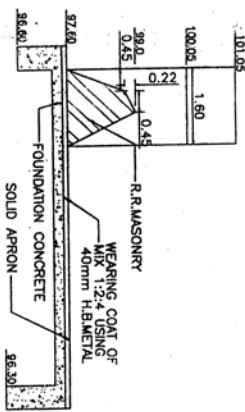


Figure A-5.1